Disturbance Rejection Control
based on Adaptive Identification of Transfer Characteristics
from Acceleration Sensor for Hard Disk Drive System

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In this paper, a new method for disturbance rejection control which is based on adaptive identification of transfer characteristics from acceleration sensor is proposed. For hard disk drive, external disturbance which should be reduced is growing with widespread use of movable computers and other independent machinery. In order to reject the effect of the external disturbance we apply the feedforward controller which is designed by the adaptive identification algorithm. In adaptive identification, the proposed method uses Disturbance Observer to get the estimated disturbance as a substitute for the system disturbance which can't be observed. By this, the proposed method can identify the transfer characteristics directly which was impossible before and can design the feedforward input easily. Some experimental results in which a hard disk drive is shaken in the vertical direction are shown to verify the effectiveness of the proposed method.

Keywords: hard disk drive, accelerometer, external disturbance rejection, feedforward control, recursive least squares algorithm, disturbance observer

1. Introduction

Control performance of hard disk drive system has been desired to be more quick and accurate for the demand of high density and capacity. As results of several researcher's efforts, hard disk drive system has achieved very high performance. But while movable computers are in widespread use, it is necessary to work well under vibrational circumstances.

In tracking control of hard disk drive system, two kinds of servos are applied, the seek mode and the following mode. In the seek mode, the head moves from the current track to the desired track. In the following mode, the head should stay in the current track to read/write data on the disk. Especially in the following mode robustness against disturbance and fluctuation of the actuator is required.

In order to improve the performance of the following mode, many methods have been proposed. Due to the development of low cost but high quality accelerometers, accelerometers can be used for compensating external and internal disturbances. White and Tomizuka proposed a feedforward controller to reduce the rotational vibration by matching the electromechanical impedance between the accelerometer and PES (Position Error Signal). Panun and Horowitz also proposed an adaptive feedforward controller using the dynamics between the accelerometer and PES. In these methods, though the effective controllers were realized, it was complicated to design because the feedforward controller was made from the transfer characteristics between acceleration and PES with involved calculation. Consequently these methods were obliged to apply in offline calculation and can't adjust to variations of product's characteristics and environmental factors like temperature.

This paper also proposes a feedforward controller with the accelerometer, too. The proposed feedforward controller differs from the existing controllers at the point that we directly use the dynamics between the accelerometer and the disturbance of the system, which can't be observed. In order to resolve this problem, we use Disturbance Observer to estimate disturbance. By utilizing the estimated disturbance, the
Fig. 2. Block diagram for access control of hard disk drive system with excitation.

Fig. 3. Transfer characteristics from acceleration sensor to disturbance of system.

In this paper, we apply two well-known algorithms, RLS algorithm and FT algorithm, to identify the transfer characteristics. Both algorithms can be formulated as (5) \sim (8).

\[ \theta(k) = \theta(k-1) + \frac{\Gamma(k-1)\varphi(k)}{1 + \varphi^T(k)\Gamma(k-1)\varphi(k)}\varepsilon(k) \]

(5)

\[ \varepsilon(k) = d(k) - \varphi^T(k)\theta(k-1) \]

(6)

\[ \Gamma(k) = \frac{1}{\lambda(k)}\{\Gamma(k-1) - \frac{\Gamma(k-1)\varphi(k)\varphi^T(k)\Gamma(k-1)}{1 + \varphi^T(k)\Gamma(k-1)\varphi(k)}\} \]

(7)

\[ \lambda(k) = 1 - \frac{\|\Gamma(k-1)\varphi(k)\|^2}{1 + \varphi^T(k)\Gamma(k-1)\varphi(k)}t_T\Gamma(0) \]

(8)

Here, \(\Gamma(k)\) is the covariance matrix, \(\theta(k)\) is the identified parameters as expressed in (9) and \(\varphi(k)\) is the signals of the input and the output of the identified transfer characteristic as in (10). In RLS algorithm the identified parameters \(\theta(k)\) is determined so that the error as (6) is minimized. In addition, using FT algorithm the parameters of the transfer characteristics can be identified properly, because FT algorithm automatically sets the forgetting factor \(\lambda(k)\) by the magnitude of the signals of the input and the output \(\varphi(k)\) as (8). Additionally a designer can set the trace of the covariance matrix \(t_T\Gamma(0)\) for renewal degree of the identified parameters \(\hat{\theta}(k)\).

By the adaptive identification online, transfer characteristics from acceleration sensor can be identified precisely even if transfer characteristics is varying, as is the case with frequency or gain of the external disturbance is time-varying.

\[ \varphi(k) = [-d(k-1), \ldots, -d(k-N_e)] \]

(9)

\[ \theta(k) = [\bar{a}_1, \ldots, \bar{a}_{N_a}, \bar{b}_1, \ldots, \bar{b}_{N_b}]^T \]

(10)

2.1 Structure of Hard Disk Drive System

Block diagram for the access control of hard disk drive system with excitation is drawn in Fig. 2. \(P\) is the actuator dynamics, \(C\) is the conventional feedback controller, \(r\) is the control reference which is usually 0 in the following mode, \(e_{\text{PES}}\) is the Position Error Signal and \(v\) is the control input to the voice coil motor. \(\xi_{\text{noise}}\) is the typical error in hard disk drive system which is consist of RRO (Repetitive RunOut) synchronous to the disk rotation and NRRO (Non-Repetitive RunOut) asynchronous to the disk rotation, which are caused by disk deflection, rotational wind and etc. The external acceleration \(a\) exerts bad influence to the system by the disk fluctuation \(d_1\) and the head fluctuation \(d_2\) through \(G_1, G_2\) which denote the dynamics between \(a\) and \(d_1, d_2\). The transfer characteristics from \(a\) to \(e_{\text{PES}}\) can be described in (2) in which \(S\) expresses the sensitivity function in (1).

\[ S = \frac{1}{1 + CP} \]

(1)

\[ e_{\text{PES}} = (G_1 + P \cdot G_2) \cdot S \cdot a \]  

(2)

Here, the transfer characteristics from the acceleration sensor to the disturbance of the system \(d\) is re-defined as \(G\) in Fig. 3 and (3). This transfer characteristics is expressed by the general discrete transfer function (ARMAX model) with limited order as in (4).

\[ G = \frac{G_1 + P \cdot G_2}{P} \]  

(3)

\[ d = G \cdot a = \frac{B(z^{-1})}{A(z^{-1})} \cdot a \]  

(4)

\[ A(z^{-1}) = 1 + a_1 z^{-1} + a_2 z^{-2} + \cdots + a_{N_a} z^{-N_a} \]

\[ B(z^{-1}) = b_1 z^{-1} + b_2 z^{-2} + \cdots + b_{N_b} z^{-N_b} \]

2.2 Adaptive Identification Algorithm

Various methods were reported to identify several systems.
Fig. 4. Block diagram of disturbance observer to estimate disturbance.

\[
\dot{d} = \left\{ -\frac{CP}{1+CP} \cdot Q + \frac{P}{1+CP} \cdot \frac{Q}{P_n} \right\} \cdot d \\
- \left\{ -\frac{C}{1+CP} \cdot Q + \frac{1}{1+CP} \cdot \frac{Q}{P_n} \right\} \cdot \{ r + \xi_{\text{noise}} \} \\
= \frac{P}{P_n} + \frac{CP}{1+CP} \cdot Q \cdot d + \frac{P}{P_n} + \frac{CP}{1+CP} \cdot \frac{Q}{P} \cdot \{ r + \xi_{\text{noise}} \} \\
\approx Q \cdot d + \xi \tag{13}
\]

From block diagram (Fig. 4), the estimated disturbance can be expressed in (11). We assumed that \( P \) is close to \( P_n \), and \( Q \) expresses the influence of the \( \xi_{\text{noise}} \) and the difference between \( P \) and \( P_n \) in (12). With the estimated disturbance \( \hat{d} \), (10) is substituted by (14). In (14), \( \hat{d} \) can be approximated to \( Q \cdot d \) from (13). Therefore by low-pass filter \( Q \) added to \( a \) to make \( Q \) and \( d \) consistent, (14) is equivalent with (10) for identification of the transfer characteristics. In identification algorithm, (6) is also substituted by (16).

By utilizing Disturbance Observer, the transfer characteristics between the acceleration sensor and system disturbance can be identified directly which was impossible in the past.

\[
\varphi'(k) = [\hat{d}(k-1), \ldots, \hat{d}(k-N_n), Q \cdot a(k-1), \ldots, Q \cdot a(k-N_n)]^T \\
\approx [-Q \cdot d(k-1), \ldots, -Q \cdot d(k-N_n), Q \cdot a(k-1), \ldots, Q \cdot a(k-N_n)]^T \\
\varepsilon(k) = \hat{d}(k) - \varphi^T(k) \hat{\theta}(k-1) \tag{16}
\]

3. Design of Feedforward Input

3.1 Principle of Feedforward Input Design

In the previous section, we proposed the adaptive identification of the transfer characteristics with Disturbance Observer. Using this transfer characteristics in (4), we can calculate the feedforward input \( u_{FF} \) with only past signals.

Generally speaking, feedforward input \( u_{FF} \) can be calculated with the identified parameters and the input and output signals in (17). But in practice, the external disturbance \( d(k) \) can't be observed directly as related before.

\[
u_{FF,1}(k) = \hat{G} \cdot a(k) \tag{17}
\]

\[
= \hat{B}(z^{-1}) a(k) + \{1 - A(z^{-1})\} d(k) \tag{18}
\]

\[
= \hat{b}_1 a(k-1) + \cdots + \hat{b}_{N_b} a(k-N_b) + \hat{a}_1 d(k-1) + \cdots + \hat{a}_{N_a} d(k-N_a) \tag{19}
\]

3.2 Practical Design of Feedforward Input

To resolve the problem in the previous section, the estimated disturbance \( \hat{d} \) can be used as a substitute for the external disturbance like identification in (20).

But, \( \hat{d} \) has considerable noise in (12), the error between \( P \) and \( P_n \), \( \xi_{\text{noise}} \) and etc. Therefore in the proposed method, since the identification is assumed to be true, the feedforward input \( u_{FF} \) itself can be used as a substitute for the external disturbance in (21).

\[
u_{FF,2}(k) = \hat{b}_1 a(k-1) + \cdots + \hat{b}_{N_b} a(k-N_b) + \hat{a}_1 u_{FF}(k-1) + \cdots + \hat{a}_{N_a} u_{FF}(k-N_a) \tag{20}
\]

Hereby, the feedforward input can be realized recursively. In this case, the feedforward input can be calculated with only acceleration signals and identified parameters. After this section \( u_{FF,2} \) is applied as the proposed feedforward input.

The external disturbance \( d(k) \) is rejected by the feedforward input \( u_{FF} \) (Fig. 5). As a merit of this proposed method, the feedforward input \( u_{FF} \) can be applied to the system without reconstruction of the system.

4. Advantage of Proposed Method

The advantages of the proposed method using Disturbance Observer are:

- Only one identification of transfer characteristics from accelerometer and disturbance
- No need to calculate any transfer functions for feedforward controller.

In the proposed method, feedforward controller can
be designed sequentially under the favor of these advantages. Moreover, the proposed method can be applied in a realtime manner due to the fast estimation of Disturbance Observer. In fact, all calculation of the proposed method including realtime identification and design of feedforward input can be completed within 168 [$\mu$s], the sampling time of the original control system. Herewith the proposed feedforward controller can adjust to variations of product’s characteristics and environmental factors like temperature.

On the contrary, in the conventional methods, several identification of transfer characteristics of system are needed because external disturbance can’t be observed directly. Besides, calculation between the transfer functions is also needed to design the feedforward controller. Therefore, the conventional feedforward controllers need to be designed by offline calculation in advance. But designed like this, the feedforward controller can’t adjust to variations of product’s characteristics and environment factors.

In the proposed method, it is possible to omit the complicated procedure and have high performance to reject the external disturbance.

5. Experiment with Hard Disk Drive

5.1 Experimental Setup  

Fig. 6 shows the configuration of the experimental system. The accelerometer is mounted on the base of a hard disk drive to measure the external disturbance and the hard disk drive is shaken by a exciter in the direction, perpendicular to the spindle motor’s axis by the sinusoidal wave which amplitude is about 2.0 [G]. Without the proposed method under excitation of such an amplitude, PES can’t be suppressed and the error the head can read/write data on the disk on the safe side. The accelerometer is installed in the direction so as to maximize the sensitivity of the accelerometer for the carriage’s movement. In these experiments, a 2.5 inch hard disk drive (36 [kTPF]) is used, for the proposed method aims at improvement of performance of movable machinery.

In each sampling time the hard disk drive sends PES and the acceleration signal to the control PC and the control PC calculates the transfer characteristics and sends $v$ and the proposed feedforward input $u_{FF}$ to the hard disk drive. The conventional feedback controller is composed of PID controller which is already tuned. All system is carried out by the sampling time of 158 [$\mu$s].

The cut-off frequency of the low-pass filter in Disturbance Observer is set to 500 [Hz]. The order of the identified parameter $\theta(k)$ are decided to $N_a = N_b = 4$ in the experiments.

5.2 Experimental Result  

To verify the effectiveness of the proposed method, specific-frequency disturbance is given to the hard disk drive. Figs. 7 ~ 12 show the experimental results. In Figs. 7, 9 and 11 the time series of PES with 60, 100 and 300 [Hz] excitation are shown. In these experiments The hard disk drive is controlled by the conventional feedback controller (0 ~ 500 [ms]) and by the conventional feedback controller including the proposed feedforward controller (500 ~ 2000 [ms]). Additionally Fourier transform of PES are shown in Figs. 8, 10 and 12 with each excitation. In these experiments, the time series of PES should be no error ideally. But in fact, for RRO and

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Fig. 7. Time series of PES with 60 [Hz] excitation.

(a) Without proposed feedforward input

(b) With proposed feedforward input

Fig. 8. Fourier transform of PES with 60 [Hz] excitation.
NRRO are existed, the time series of PES have vibrational error in high frequency band within an allowance. As below, control performances against each frequency disturbance are discussed.

5.2.1 Control Performance against Low Frequency Disturbance  Figs. 7, 8 show the experimental results for 60 [Hz] disturbance. For low frequency disturbance (∼80 [Hz]), conventional feedback controller can suppress the disturbance well. After applied the proposed feedforward controller, the proposed controller can additionally suppress the 60 [Hz] excitation without harm to performance of the conventional feedback controller (Fig. 8).

5.2.2 Control Performance against Middle Frequency Disturbance  Figs. 9, 10 show the experimental results for 100 [Hz] disturbance. For middle frequency disturbance (90 ∼ 200 [Hz]), the conventional feedback controller can't suppress disturbance because the frequency of disturbance goes beyond the controllable band of the conventional feedback controller. On the contrary, after applied the proposed feedforward controller, middle frequency disturbance can be suppressed remarkably.

5.2.3 Control Performance against High Frequency Disturbance  Figs. 11, 12 show the experimental results for 300 [Hz] disturbance. In high frequency disturbance (300 [Hz] ∼), though the frequency of disturbance goes beyond the controllable band of the conventional feedback controller, disturbance influence doesn't appear strongly because the transfer func-
6. Conclusion

In this paper, we proposed a novel method for the external disturbance rejection control, based on the adaptive identification of transfer characteristics from acceleration sensor for access control of hard disk drive system. In this method, we can identify the transfer characteristic from acceleration sensor with Disturbance Observer and design the feedback controller. In the experiments, a 2.5 inch hard disk drive (36 [kTPI]) is shaken, but PES is reduced by the proposed feedback controller, especially in middle frequency band that the conventional feedback controller can't perform sufficiently. As a result of this experiments, we can design the proposed feedback controller in online calculation and verify the effectiveness of the proposed feedback controller. Recently, hard disk drive is used not only for computers but also for other machinery to utilize the performance and the capacity of hard disk drive. In the future this tendency is expected to continue and therefore hard disk drive against disturbance is significant subject of research.

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