Microstructure and ferroelectric properties of spark plasma sintered Li substituted $K_{0.5}Na_{0.5}NbO_3$ ceramics

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Potassium sodium niobate (KNN) is a well known piezoelectric material and a developing candidate for replacing lead based high performance piezoceramics due to limitations of hazardous materials in electronic devices. Lithium substitution in KNN structure leads a crystal transition from orthorhombic to tetragonal symmetry at room temperature and enhances ferroelectric properties. In this study, lithium substituted KNN piezoceramics with high relative densities were prepared by spark plasma sintering (SPS). Densification, crystal structure, microstructure and ferroelectric behavior of the samples were investigated. It was observed that lithium niobate based secondary phases exist in sintered KNN ceramics. These secondary phases showed significant effects on ferroelectric properties. Maximum ($P_u$) and remnant ($P_r$) polarizations were determined as 27 and 20 $\mu$C/cm$^2$, respectively for pure KNN at the electric field of 20 kV/cm. When the electric field was increased to 30 kV/cm, $P_u$ did not change significantly, but remained below $P_r$. For Li substituted samples, $P_r$ decreased with increasing Li content.

Key-words : Lead free piezoceramics, Niobates, Perovskites, Sintering, Ferroelectric properties

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1. Introduction

PZT (PbZrTiO$_3$) is a piezoelectric crystal which has a wide spread usage as ultrasonic transducers, sensors and actuators. However, harmful effects of Pb content on environment promotes a pursuit of new high performance lead-free perovskite crystals. Potassium Sodium Niobate (KNN) is a well known lead-free piezoelectric ceramic material which is a solid solution of NaNbO$_3$ and KNbO$_3$. Until a few years ago, there have been only a few reports about the piezoelectricity of NaNbO$_3$, KNbO$_3$ and NaNbO$_3$–KNbO$_3$ ceramics which exhibit an important combination of electrical and mechanical properties and environmentally friendly character, probably because of their poor sinterability and the high volatility of the sodium and potassium components during sintering at high temperatures and long sintering times. For alkaline niobate ceramics, accurate process control is required in order to obtain compositional homogeneity. These challenges could be accomplished by using the SPS technique. In this technique, a compact powder can be sintered to high density under a uniform heating at relatively lower temperatures and in much shorter sintering periods compared with other sintering methods including pressure sintering, hot pressing, and/or hot isostatic pressing.\(^{2-4}\)

In the SPS process, a pulsed direct current passes through a graphite punch rods and dies simultaneously with a uniaxial pressure. The microstructure and volatilization of sodium and potassium can be controlled by a fast heating rate and shorter processing times.\(^{5}\)

It was reported that, pure KNN sintered with SPS have a compatible bulk density with hot press, as 4.48 Mg/m$^3$.\(^{2,16,17}\) Also, it is possible to modify crystal structure of KNN with several dopants in order to obtain higher ferroelectric and piezoelectric properties. LiNbO$_3$, SrTiO$_3$, LiTaO$_3$ and LiSbO$_3$ are mostly substituted compounds.\(^{7-11}\) The highest piezoelectric properties of KNN can be obtained close to morphotropic phase boundary (MPB) at a composition where K/Na ratio approximates 1.\(^{1}\) MPB states the existence of two different crystal structures together.\(^{12,13}\) KNN is in orthorhombic crystal structure at room temperature and it has orthorhombic-tetragonal crystal transition at 224°C.\(^{14}\) Compared to orthorhombic phase, tetragonal KNN represents favorable piezoelectric features due to its higher crystal symmetry. Lithium substitution distorts the orthorhombic unit cell and originates the constitution of a far amount of tetragonal crystal phase in KNN representing MPB at room temperature.\(^{12-15}\) There are few papers in literature about lithium substituted potassium sodium niobate (KLNN) type ceramics which were produced using SPS technique.\(^{15,16}\)

In this study, the effects of Li substitution on the microstructural and ferroelectric properties of spark plasma sintered ($K_{0.5}N_{0.5})_1-x Li_x$NbO$_3$ ceramics (KLNN) were investigated.

2. Experimental

Commercial lithium carbonate (Li$_2$CO$_3$, Merck, 99.0%), sodium carbonate (Merck, 99.9%, Na$_2$CO$_3$), potassium carbonate (K$_2$CO$_3$, Merck, 99.0%) and niobium oxide (Nb$_2$O$_5$, Alfa-Aesar, 99.9%, 325 mesh) were used as starting powders for synthesis of Li modified KNN powders via favorable route called as mixed oxides solid state reactions.\(^{17}\) These hygroscopic materials were kept in an oven at 96°C to avoid absorption of water. Oxide and carbonates were balanced in stoichiometric ratio, then ball milled in a polyethylene bottle (Nalgene, 250 ml) for 24 h at 210 rpm using ethanol media with a mixture of YSZ balls in different diameters. Homogeneously milled and mixed composition were calcined at 850°C for 2 h with a heating rate of 5°C/min. Different compositions of ($K_{0.5}N_{0.5})_1-x Li_x$NbO$_3$ (where x = 0, 2, 4, 6, 8 and 10) were prepared by using this route.

A graphite die 50 mm in inner diameter was filled with the calcined powder mixtures, followed by sintering using SPS apparatus (SPS-7.40 MK-VII, SPS Syntax Inc.) at 980–1085°C.
for 180 s with a heating rate of 1.7°C/s in a vacuum. A graphitic sheet was placed between the punches and the powder, and between the die and the powder for easy removal and better conductivity. A uniaxial pressure of 40 MPa and a pulsed direct current (12 ms on, 2 ms off) were applied during the entire SPS process. The uniaxial pressure was released during cooling for all samples. An optical pyrometer, focused on a small hole at the surface of the graphite die, was used to measure and adjust the temperature. The current was controlled manually, and linear shrinkage of the specimens during SPS process was continuously monitored by displacement of the punch rods. Maximum density was generally achieved when the shrinkage of specimen was stopped at a certain temperature. Thus, in this study, final sintering temperature for each composition was determined at the temperature when the shrinkage stopped. The effect of thermal expansion of the graphite punch rods with increasing temperature on displacement of the specimens was negligible. The initial thickness of powder compacts was approximately 7 mm and reduced to 4 mm at the end of the sintering process. The sintered specimens were in the form of pellets 50 mm in diameter and 4 mm thick and characterized after sand-blasted in order to remove the graphitic sheet.

After sintering process, heat treatments were applied to all samples at 900°C for 30 min in an open atmosphere in order to remove the residual stresses which were originating from fast sintering process of SPS. Annealing period was kept as short as possible to avoid grain growth. The bulk densities of the specimens were measured by the Archimedes’ method and converted to relative density by using theoretical densities. The fractured surfaces of the specimens were investigated by field emission scanning electron microscope (JEOL JSM 7000F, Japan) with an acceleration voltage of 10 kV. The crystalline phases and crystallographic analyses of the annealed ceramics were performed by X-ray diffractometry (Rigaku Miniflex, Japan) in the 2θ range of 10–80° with Cu Kα radiation. For the investigation of ferroelectric properties, samples were prepared with a thickness of 1.5 mm using mechanical polishing and polished surfaces were coated with silver paste. The silver paste was fired at 650°C for 30 min.

Ferroelectric properties of synthesized ceramics with different compositions were investigated with ferroelectric material test system (Radiant Precision LC Ferroelectric test system, U.S.). Different polarization electric field intensities and cycle periods were used to perform the tests of ferroelectric behavior of different KLNN compositions.

3. Results and discussion

3.1 Phase analysis and crystallography

Figure 1 shows the XRD patterns of KNN and KLNN specimens sintered at 975–1090°C for 180 s. KNN phases were identified using orthorhombic KNbO3 (JCPDS: 32-0822) phase due to the lack of K0.5Na0.5NbO3 solid solution card. This phase is a member of family of perovskite structures which is formulated as ABO3 where A and B denote the atoms invade the corners and body centered positions of a unit cell respectively.13)

Pure KNN was well suited to diﬀraction pattern of forssaid KNbO3 phase representing fully orthorhombic structure. A slight shifting in peak positions was also observed and evaluated as originating from replacement of K with Na ions in the unit cell.

For the Li substituted samples, relative intensities of the peaks originating from the atomic planes (100), (200), (210), (211) of tetragonal phase increased steadily with increasing Li content. Furthermore, peaks of (101) and (110) planes became visible at diffraction pattern of 8% Li substituted sample. Tetragonal KNN phases were identiﬁed using tetragonal KNbO3 phase (JCPDS: 71-0945). These circumstances pointed out the crystallographic transition from orthorhombic to tetragonal symmetry, and the tetragonal to orthorhombic phase ratio increased with increasing Li substitution.

Li atoms replaced the A sites in ABO3 sub-cell of perovskite structure and this replacement caused a large distortion in the unit cell due to the difference in the atomic radius of Li.13) It was concluded that, a mixture of the orthorhombic and tetragonal phases existed in the samples of 2, 4 and 6% Li substituted. The KLNN samples with 8 and 10% Li were identiﬁed as fully tetragonal.

Figure 2 shows the extended X-ray diﬀraction patterns in the 2θ range of 20–50° for all compositions. Several secondary crystalline phases were identiﬁed for all compositions. For pure
KNN, two peaks were appeared at positions between 32.5 and 35°. These peaks were considered as secondary crystalline phases of NaNbO₃ (JCPDS: 37-1076) and KNbO₃ (JCPDS: 31-1058). Other possible peak-positions belong to these phases were also indicated on diffraction pattern. One more secondary crystalline phase which had a diffraction peak at about 2θ = 28.5° was identified and any alkali niobe phase except K₃NbO₄ (JCPDS: 52-1895) could not be suited or found close to observed diffraction pattern. A small shift to lower 2θ values was observed in expected peak position of aforesaid potassium niobe phase and this peak was assumed to belong to K₃NbO₄ based structure with a distorted unit cell. The potassium niobe based structure became obvious while two secondary phases of NaNbO₃ and KNbO₃ disappeared in the diffraction pattern of 4% Li substituted samples which were shown in Fig. 2(c). The hexagonal LiNbO₃ (JCPDS: 20-0631) crystalline phase was identified in XRD pattern of 6% Li substituted in addition to K₃NbO₄ based structure [Fig. 2(d)]. This sample was also determined as the mixture of tetragonal and orthorhombic KNN phases. This result revealed that, hexagonal LiNbO₃ phase crystallized simultaneously with KNN phase under solubility limit of Li in KNN. For the sample of 8% Li substituted, the
relative intensity of LiNbO$_3$ phase increased [Fig. 2(c)] and a new secondary crystalline phase was identified which assumed to belong to a body centered cubic Li$_2$NbO$_4$ (JCPDS: 16-0459). In the XRD pattern of the sample with 10% Li substituted [Fig. 2(f)], LiNbO$_3$ phase disappeared and the relative intensity of Li$_2$NbO$_4$ phase increased. Furthermore, a diffraction peak appeared at 2$\theta$ = 25.5° and no alkali niobate phase could be suited except K$_3$Li$_4$Nb$_{12}$O$_{25}$ (JCPDS: 52-0157). The most intense peak formation of this phase at 2$\theta$ = 22.4° could have been caused by overlapping with KLN phases.

The densification of the specimens during SPS process was evaluated by the displacement of punch rods due to shrinkage of the samples. Figure 3 shows the displacement of KNN and KLNN ceramics and isothermal shrinkage behavior at sintering temperatures for 180 s. Final sintering temperature was determined at the temperature when the shrinkage stopped.

The shrinkage of pure KNN started at 765°C and completed at 1000°C. The starting temperature of shrinkage increased with increasing Li content up to 4%. For the specimen with 2 and 4% Li, starting temperatures of shrinkage were determined as 800 and 850°C, respectively. The lowest starting temperature of shrinkage (775°C) was observed with 6% Li substituted specimens, and showed similar shrinkage behavior with pure KNN. For the specimens with 8 and 10% Li, shrinkage started at 800 and 840°C, respectively. For these samples, shrinkage completed at 1000 and 1050°C.

Different starting and completion temperatures of shrinkage could be explained by the formation of different secondary phases. Temperatures of shrinkage and relative densities of KNN based ceramics are given in Table 1. For pure KNN, main phases were NaNbO$_3$ and KNbO$_3$ with melting temperatures of 1400 and 1080°C, respectively. The content of these two phases decreased for 2% Li substituted sample and was not observed for the KLNN sample containing 4% Li. Disappearance of these two alkali niobate phases was attributed to higher sintering temperatures, 1050 and 1090°C, which possibly induced reactions between these phases producing KNN. Since the melting temperature of LiNbO$_3$, 1257°C, was lower than that of NaNbO$_3$, for the sample 6% Li substituted, the sintering temperature was determined as the lowest, 975°C, due to the disappearance of this secondary phase. The formation of high melting temperature Li$_2$NbO$_4$, 1408°C, resulted in both high starting and completion temperatures for 8 and 10% Li substituted samples. The relative densities of the samples (Table 1) slightly decreased with increasing Li content. The relative density of pure KNN was about 99.9%, while that of specimen with 10% Li reached 98.8%. These results are compatible with hot pressed ceramics given in literature. It was considered that, followed sintering method, i.e. controlling the shrinkage behavior continuously, was favorable to achieve high density KLNN ceramics, when these results were compared with the similar reported studies in which a constant sintering temperature was applied for all compositions.

### Table 1. Effect of Li content on relative density, starting and completing temperatures of shrinkage

<table>
<thead>
<tr>
<th>Composition</th>
<th>Relative density (%)</th>
<th>$T_s$ (°C)</th>
<th>$T_f$ (°C)</th>
</tr>
</thead>
<tbody>
<tr>
<td>K$<em>3$Na$</em>{0.5}$NbO$_3$</td>
<td>99.9</td>
<td>765</td>
<td>1000</td>
</tr>
<tr>
<td>(K$<em>3$Na$</em>{0.5}$)$<em>{0.93}$Li$</em>{0.07}$NbO$_3$</td>
<td>99.7</td>
<td>800</td>
<td>1050</td>
</tr>
<tr>
<td>(K$<em>3$Na$</em>{0.5}$)$<em>{0.91}$Li$</em>{0.09}$NbO$_3$</td>
<td>99.5</td>
<td>850</td>
<td>1090</td>
</tr>
<tr>
<td>(K$<em>3$Na$</em>{0.5}$)$<em>{0.9}$Li$</em>{0.1}$NbO$_3$</td>
<td>99.2</td>
<td>775</td>
<td>975</td>
</tr>
<tr>
<td>(K$<em>3$Na$</em>{0.5}$)$<em>{0.8}$Li$</em>{0.2}$NbO$_3$</td>
<td>99.2</td>
<td>800</td>
<td>1000</td>
</tr>
<tr>
<td>(K$<em>3$Na$</em>{0.5}$)$<em>{0.7}$Li$</em>{0.3}$NbO$_3$</td>
<td>98.8</td>
<td>840</td>
<td>1050</td>
</tr>
</tbody>
</table>

3.2 Microstructure

Microstructural of fracture surfaces of the samples with compositions of (K$_3$Na$_{0.5}$)$_{1-x}$Li$_x$NbO$_3$ (x = 0–10) are shown in Fig. 4. The microstructure of the pure KNN consisted of rectangular shaped grains 1–5μm in size [Fig. 4(a)]. The fracture mechanism was mainly intergranular. Figure 4(b) shows the microstructure of the sample with 2% Li. Grain size was determined about 2μm and fracture took place in the grains. For 4% Li substituted KNN sample grain size was determined about 5μm [Fig. 4(c)]. For the specimens containing 6, 8 and 10% Li, grains were in perfect rectangular shapes. The grain size exceeded 15μm for the sample containing 10%. Although SPS method enables to control the grain growth mechanism, a significant enlargement in grain size was observed. This result pointed out the grain growth of this sample could be due to high lithium substitution. Probably lithium niobate with high melting point or potassium lithium niobate secondary phases show seeding effect.

A remarkable cleavage behavior was observed for 8% Li substituted sample. The magnified view of fracture surface of this sample is shown in Fig. 5. The periodic bright and darker fields in a shape of narrow strips appeared on fracture surface of a...
These oriented fields were assumed to be ferroelectric domains in opposite orientations, which showed different fracture behavior like polished and etched KNN surfaces. It was reported that in the literature, ferroelectric domains of a KNN single crystal was clearly observed by using SEM method from polished sample. It is clear in Fig. 5, two different orientation directions (normal to the strips) existed and these directions were indicated with white arrows. Some of the brighter (white lines) and darker fields (black lines) in different orientation directions were indicated. The angle between red lines in different directions was determined as 90°. It was considered that, 90° domain boundary took place between these strips which were in different orientation direction and white dotted line signed on the micrograph indicated that the location of possible 90° domain boundary. Also 180° domain boundaries were evaluated taking placed between brighter and darker fields, but it is impossible to show polarization directions without taking
diffraction pattern from these domains using high resolution transmission electron microscopy (HRTEM) method. These two type domain boundaries were evaluated as common for whole grain and any other orientation was not observed. These assumptions were also in agreement with the results of crystallographic investigation for 8% Li substituted composition which was fully tetragonal. It was referred in literature, only 90 and 180° domain boundaries exist for tetragonal perovskite structures. For orthorhombic perovskites, 60 and 120° domain boundaries can be constituted in addition to 90 and 180° domain

Fig. 6. Hysteresis loops of (a) non-substituted KNN, (b) 2%, (c) 4%, (d) 6%, (e) 8%, (f) 10%, Li substituted KNN ceramics.
3.3 Ferroelectric properties

The polarization behavior of \((K_{0.5}Na_{0.5})_{1-x}Li_xNbO_3\) was observed under various electric field intensity and cycle periods. For pure KNN, polarization curves were obtained at the electric field of 30 kV/cm. Dielectric break-down was occurred when this electric field intensity value was exceeded for this sample. Other samples polarized at the electric field of 40 kV/cm and hysteresis curves were sketched. This electric field intensity value was determined as saturation point for maximum polarization. Hysteresis curves of the samples are shown in Fig. 6. Maximum remnant polarization were determined as 27 and 20 \(\mu C/cm^2\), respectively for pure KNN sample at the electric field of 20 kV/cm. For larger electric field intensities, remnant polarization was determined to be larger than that of maximum polarization for not substituted KNN sample. This result was attributed to leakage contribution. Existence of anti-ferroelectric sodium niobate phase may have some contribution on rounded hysteresis loops. Total spontaneous polarization of this anti-ferroelectric phase under applied electric field was zero and any extra effect originating from this phase did not contribute to the maximum polarization value. The dipoles of this phase aligned parallel to dipoles of KNN and originated the enlargement of polarization while quenching the electric field. This effect was reported before in literature.\(^{21}\) The polarization behavior of the 4 and 6% Li substituted samples are shown in Figs. 6(c) and 6(d), respectively. Maximum polarization values of these samples were measured at the electric field of 40 kV/cm for 300 ms cycle period. Maximum polarization values were obtained as 24 and 26 \(\mu C/cm^2\) respectively for the 4 and 6% Li substituted samples. It was observed that, remnant polarization values reduced with increasing Li content. Small nails appeared on hysteresis curves of 2 and 4% substituted samples [Figs. 6(b) and 6(c)]. This behavior pointed out that, 300 ms was insufficient as a cycle period. The composition of \((K_{0.5}Na_{0.5})_{1-x}Li_xNbO_3\) represented an optimal ferroelectric behavior [Fig. 6(d)]. Furthermore, a degradation hysteric behavior was pointed out electrical conductivity for the samples containing 8 and 10% Li [Figs. 6(e) and 6(f)]. Degradation in hysteresis loop could be originating from the existence of cubic \(Li_3NbO_3\) secondary phase more than tetragonal \(LiNbO_3\) for the samples containing 8 and 10% Li. \(LiNbO_3\) is a well known ferroelectric crystal and existence of this secondary phase in 6% Li substituted KNN shows no degradation in hysteresis loops. Ferroelectric \(LiNbO_3\) phase may have extra dipole contribution to polarization.

4. Conclusions

Li modified KNN lead-free piezoelectric ceramics were prepared by spark plasma sintering. Using current controlled sintering method made it possible to reach high relative densities up to 99.9%. Secondary phases revealed in KNN ceramics which has a significant contribution to ferroelectric properties besides of orthorhombic to tetragonal phase transition. Lithium niobate phase in cubic crystal structure (\(Li_3NbO_3\)) degrades hysteretic behavior.

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References