Effects of Excess Mg and Si on the Isothermal Ageing Behaviours in the Al–Mg2Si Alloys

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The effects of excess Mg and Si contents on the isothermal ageing processes of Al-Mg2Si alloys have been investigated by means of transmission electron microscopy and the following results were obtained. After the formation of $\beta'$ needles inducing large age hardening, cuboid $\beta$ particles precipitate in both the excess Mg and the quasi-binary alloys, but fine Si particles nucleate in the excess Si alloys. In the quasi-binary alloy, the following reaction is the precipitation of $\beta''$ rods and then $\beta''$ plates form. In the excess Si alloys, various rodlike precipitates form after the precipitation of $\beta'$ needles and Si particles in the sequence: Type-A rods $\rightarrow$ Type-B rods $\rightarrow$ $\beta''$ rods. This precipitation sequence can be understood by considering the chemical compositions of them determined by Matsuda et al.

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1. Introduction

The phases precipitating in Al–Mg2Si quasi-binary alloys have been reported as monoclinic $\beta''$ needles, hexagonal $\beta'$ rods and $\beta$-Mg2Si plates.1–6 In addition to these particles, some other intermediate phases precipitate. Cuboid $\beta$-Mg2Si particles7,8 have been frequently observed in the alloys containing excess Mg atoms and also in the quasi-binary alloys. In the excess Si alloys, however, Matsuda et al. reported that Type-A, B and C particles9–12 form as well.

The crystal structures of intermediate phases can be summarised as follows. For $\beta''$ phase, the results so far reported are rather diversified.11,13–17 Wahi et al.14 reported that the structure was monoclinic with the lattice parameters $a = 0.616\,\text{nm}$, $b = 0.710\,\text{nm}$ and $\beta = 82^\circ$. According to Lynch et al.,15 however, the lattice parameters were determined as: $a = 0.300$, $b = 0.330$, $c = 0.400\,\text{nm}$ and $\gamma = 71.00^\circ$. On the other hand, Andersen16 examined $\beta''$ phase needles by means of high-resolution transmission electron microscopy (HRTEM) and reported that the structure and its space group are monoclinic with the lattice parameters $a = 1.516$, $b = 0.405$, $c = 0.674\,\text{nm}$ and $\beta = 105.30^\circ$, and C2/m, respectively. Matsuda et al.17 obtained the lattice parameters $a = 0.77$, $b = 0.67$, $c = 0.203\,\text{nm}$ and $\gamma = 75^\circ$ by HRTEM analysis and determined the space group as P2/m. The result almost similar to that by Matsuda was also obtained by Maruyama et al.,17 i.e., the lattice parameters are $a = 0.714$, $b = 0.658$, $c = 0.405\,\text{nm}$ and $\gamma = 75^\circ$, and the space group is P2/m.

On the structure of $\beta'$ phase, Jacobs23 showed that the $\beta'$ phase has a hexagonal unit cell with the lattice parameters $a = 0.705$ and $c = 0.405\,\text{nm}$. In the same temperature range where $\beta'$ rods form, Matsuda et al. reported that Type-A, B and C rods form in excess Si alloys.9–12 The structure of Type-A phase is hexagonal with $a = 0.405$ and $c = 0.67\,\text{nm}$, that of Type-B is orthorhombic with $a = 0.684$, $b = 0.793$ and $c = 0.405\,\text{nm}$, and Type-C phase has a hexagonal unit cell with $a = 1.04$ and $c = 0.405\,\text{nm}$.

Although the precipitation reactions in Al–Mg–Si alloys have been the subjects of numerous investigations, most of them are concerned with either a specific specimen or certain ageing conditions and the effects of chemical composition, ageing temperature and time on the precipitation of various intermediate phases processes during isothermal ageing have not been fully understood. Thus, in the present study, precipitation sequences of intermediate phases during isothermal ageing in the Al–Mg2Si alloys are examined by means of conventional transmission electron microscopy (TEM).

2. Experimental Procedures

The chemical compositions of the Al–Mg–Si alloys used are shown in Table 1. The ingots were homogenised at 560°C for 12 h and were rolled to 1 mm thick plates at room temperature. In order to discuss the effects of solutionising on the precipitation processes, the chemical compositions of the present alloys were compared with the solubility limit of $\beta$-Mg2Si in $\alpha$-solid solution at 560°C (Fig. 1). The specimens machined from the plates of the alloys 2, 4 and 6 were solution-treated at 560°C for 30 min and quenched into iced water. Those of the alloys 1, 3, 5 and part of the alloy 4 specimens were solutionised at 590°C for 30 min. These specimens were aged isothermally in an alloy bath kept at temperatures from 150 to 350°C immediately after the quenching.

<table>
<thead>
<tr>
<th>Mark</th>
<th>Mg</th>
<th>Si</th>
<th>Mg2Si</th>
<th>Excess Si</th>
<th>Excess Mg</th>
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</thead>
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<tr>
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<tr>
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<td>0.47</td>
<td>1.23</td>
<td>0.06</td>
<td>—</td>
</tr>
<tr>
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<td>0.90</td>
<td>1.80</td>
<td>0.30</td>
<td>—</td>
</tr>
<tr>
<td>Alloy 6</td>
<td>0.93</td>
<td>1.03</td>
<td>1.39</td>
<td>0.57</td>
<td>—</td>
</tr>
</tbody>
</table>

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were carried out for the specimens aged at various temperatures. Thin foils for TEM were prepared by electrolytic polishing in the mixture of three parts of methanol and one part of HNO₃ at −30°C and were examined in a JEOL-2000EX microscope operating at 200 kV.

3. Experimental Results

3.1 Vickers hardness measurements

Figures 2(a) to (c) show the variations of Vickers hardness with ageing time for the excess Mg alloy 2, the quasi-binary Al–Mg₂Si alloy 4 and the excess Si alloy 6 aged at temperatures between 185 and 245°C after the solution treatments at 560°C, respectively. The hardness variations during isothermal ageing for the excess Mg alloy 1, the quasi-binary alloy 4 and the excess Si alloy 5 solutionised at 590°C are also shown in Fig. 3. The ageing temperatures in this case are 150, 200 and 250°C. All the specimens exhibited a similar hardening sequence. The maximum hardness values, however, exhibit quite complicated compositional dependence. In the case of solutionising at 560°C, the maximum hardness increased with increasing the excess Si content. The alloys solution-treated at 590°C exhibited the maximum hardness much higher than those solutionised at 560°C. It should be noted that even the hardness of the quasi-binary alloy 4 which can be completely solutionised at 560°C as in Fig. 1 is increased by ageing at 590°C (compare Fig. 2(b) with Fig. 3(b)) and that both the excess Mg and Si contents increase the peak hardness in comparison with that of the quasi-binary alloy in the case of 590°C solution-treatment.

3.2 TEM observation

3.2.1 The precipitation of intermediate phases in the excess Mg alloy

In the specimen aged at 210°C, very fine β‴ needles began to precipitate in accordance with the sharp hardening. Well-
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3.1.1 The precipitation of intermediate phases in the excess Mg alloy 2

Fig. 4 Precipitation of cuboid $\beta$ particles at a grain boundary in the excess Mg alloy 2 aged at 210°C for 5 h. Arrows indicate cuboid $\beta$ particles.

defined reflections from $\beta''$ needles, however, were not obtained at the initial stage of ageing. By ageing the alloy 2 at 210°C for 5 h, cuboid $\beta$ particles precipitating on grain boundaries were clearly observed in addition to the $\beta''$ needles within the matrix (Fig. 4). In the specimens aged for 50 h at 210°C, the reflections from $\beta''$ needles became much clearer. The bright field image, the selected area electron diffraction pattern and the dark field image using a $\beta''$ reflection are shown in Figs. 5(a), (b) and (c), respectively. The reflections from $\beta''$ needles can be indexed by using the lattice parameters determined by Andersen. All the reflections and the orientation relationships between the $\beta''$ needles and the $\alpha$-matrix obtained in the present study were always in keeping with the structural model by Andersen. The $\beta''/\alpha$-matrix (Al) relationships determined for $\beta''_1$ and $\beta''_2$ in the pattern Fig. 5(b) are very close to two different variants of that by Andersen:

$$
\begin{align*}
[010]_{\beta''} & \parallel [001]_{\alpha\text{Al}} \ldots \ldots \text{growth direction}, \\
(001)_{\beta''} & \parallel (320)_{\alpha\text{Al}}, \quad (100)_{\beta''} \parallel (130)_{\alpha\text{Al}}
\end{align*}
$$

The above relationship is exactly satisfied between $\beta''_1$ and the matrix. In a different area of the same specimen, cuboid $\beta$ particles were also observed within the matrix as in Fig. 6(a). The selected area electron diffraction pattern indicates that the cuboid $\beta$ particles were related to the Al matrix with the cube-cube orientation relationship. The additional reflections in the pattern arose from the double diffraction between the $\beta$ particles and the matrix. In the later stages of ageing at this temperature, $\beta'$ rods were occasionally observed.

Although the precipitation time was largely accelerated, a similar precipitation sequence was also observed in the case of ageing at 245°C. The precipitates formed by further ageing at higher temperatures were mostly $\beta$ phase particles. The formation of Type-A, B and C rods could not be observed.

3.2.2 The precipitation of intermediate phases in the quasi-binary alloy

Fig. 7 shows the $\beta''$ precipitation in the quasi-binary alloy 4 aged at 245°C for 2 h. The dark field image using $(2\bar{1}2)_{\beta''}$ and $(\bar{2}\bar{1}2)_{\beta''}$ reflections and the selected area electron diffraction pattern are illustrated in Figs. 7(a) and (b), respectively. The diffraction pattern involved four variants of Andersen’s $\beta''/\text{Al}$ orientation relationship described above. In a different area of the same specimen, cuboid $\beta$ particles were observed as shown by arrows in Fig. 8. These $\beta$ particles were also related to the matrix by the cube-cube orientation relationship. By further ageing at the same temperature, $\beta'$ rods having a hexagonal crystal lattice precipitated. Figures 9(a) and (b) are the bright field image and the selected area electron diffraction pattern for the specimen aged at 245°C for 190 h. $\beta'$ rods elongated in the $(100)_{\alpha\text{Al}}$ directions can be seen. The lattice parameters used for the analysis are due to those obtained by Jacobs. The orientation relationship in this
Fig. 6 $\beta''$ needles and cuboid $\beta$ particles in the excess Mg alloy 2 aged at 210°C for 50 h. (a) Bright field image using the (220)$_{\beta}$ reflection, (b) the selected area electron diffraction pattern and (c) the dark field image using the (220)$_{\beta}$ reflection.

This case can be expressed as:

$$[0001]_{\beta'} \parallel [100]_{Al} \cdots \cdots \text{growth direction},$$

$$(01\bar{1}0)_{\beta'} \parallel (031)_{Al}, \ (2\bar{1}10)_{\beta'} \parallel (0\bar{1}3)_{Al}$$

This relationship is in good agreement with that referred to as "middle range type" by Matsuda et al. 19) within an experimental error. In the specimens aged at 300°C, the precipitation of Mg$_2$Si $\beta$ plates and $\beta'$ rods were recognised. Figure 10(a) shows the $\beta$ plates formed in the specimen aged at 300°C for 2 h. The habit plane of the plates is parallel to [100]$_{Al}$ matrix plane but the edges of the plates incline about 18° from (100)$_{Al}$ matrix directions as can be seen in the diffraction pattern (b). The orientation relationship between this plate and the matrix is very close to:

$$(001)_{\beta} \parallel (001)_{Al} \cdots \cdots \text{habit plane},$$

$$(100)_{\beta} \parallel (3\bar{1}0)_{Al}, \ (010)_{\beta} \parallel (130)_{Al}.$$ 

This agrees well with one of the relationships observed previously. 8) The edges of the plates are parallel to the (110)$_{\beta}$
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Fig. 9 Precipitation of $\beta'$ rods in the quasi-binary alloy 4 aged at 245°C for 190 h. Arrow indicates $\beta'$ rod and double reflections are shown by "d". (a) Bright field image and (b) the selected area electron diffraction pattern.

3.2.3 The precipitation of intermediate phases in the excess Si alloys

The precipitation sequence in the excess Si alloys was significantly different from those in the excess Mg and the quasi-binary alloys as has been reported originally by Matsuda et al. and various phases were also observed in the present study. In the alloy 6 aged at 210°C for 2 h, $\beta''$ needles and fine dot-like particles were observed. Increasing the ageing time to 50 h, the particles induced well-defined reflections. Figures 12(a), (b) and (c) are the bright field image of the alloy 6 aged at 210°C for 50 h, the selected area electron diffraction pattern and the dark field image using the (111) Si reflection, respectively. The diffraction pattern (b) consists of the reflections from the matrix, those from $\beta''$ needles and those from Si particles. The orientation relationship between $\beta''$ needles and the matrix was determined by using one of the net patterns from $\beta''$ needles as shown by the broken lines in the pattern, and was confirmed to be exactly the same as the Andersen’s relationship described above. The net pattern comprising well-defined reflections and solid lines, however, was indexed as those from Si particles. The dark field illumination using a Si reflection indicates that fine Si particles with the same orientation dispersed in the specimen as shown in Fig. 12(c). The orientation relationship between Si particles and the matrix is given as:

$$(\bar{1}10)_{\text{Si}} \parallel (\bar{1}10)_{\text{Al}}, \ (111)_{\text{Si}} \parallel (110)_{\text{Al}}, \ (\bar{1}I2)_{\text{Si}} \parallel (001)_{\text{Al}}$$

This is quite far from the relationship determined by Matsuda et al.:

$$(111)_{\text{Si}} \parallel (001)_{\text{Al}}, \ [\bar{1}10]_{\text{Si}}10° \text{ from } [010]_{\text{Al}}$$

The isothermal holding at 210°C for longer times induced the precipitation of Type-A rods with diameters as large as 30–80 nm in addition to $\beta''$ needles. Figure 13(a) shows both the longitudinal figure and the cross section of Type-A rods in the excess Si alloy 5 aged at 210°C for 150h. The diffraction patterns in Fig. 13(b) indicate that the Type-A/matrix orientation relationships were very close to the two different variants of the orientation relationship determined by Matsuda et al. and can be expressed as:

$$[\bar{2}1\bar{2}0]_{\text{A}} \parallel [0\bar{1}0]_{\text{Al}} \ldots \ldots \text{growth direction},$$

$$[0001]_{\text{Al}} \parallel (301)_{\text{Al}}, \ (\bar{1}010)_{\text{Al}} \parallel (\bar{1}03)_{\text{Al}}$$

$$[\bar{2}1\bar{1}0]_{\text{A}_2} \parallel [001]_{\text{Al}} \ldots \ldots \text{growth direction},$$

$$[0001]_{\text{A}_2} \parallel (\bar{3}10)_{\text{Al}}, \ (0\bar{1}10)_{\text{A}_2} \parallel (310)_{\text{Al}}.$$
Fig. 11 Precipitation of $\beta'$ rods in the quasi-binary alloy 4 aged at 300°C for 10 h. Arrow indicates $\beta'$ rod. (a) Bright field image and (b) the selected area electron diffraction pattern.

Fig. 12 Precipitation of Si particles and $\beta''$ needles in the excess Si alloy 6 aged at 210°C for 50 h. (a) Bright field image, (b) the selected area electron diffraction pattern and (c) the dark field image using the (111)$_{\text{Si}}$ reflection.

Directions are parallel to $\langle 100 \rangle_{\text{Al}}$ as in Fig. 14(a), and the needles elongated in the $[001]_{\text{Al}}$ direction provided the diffraction pattern of $\beta''$ phase shown in Fig. 14(b). The $\beta''$/matrix orientation relationship can be expressed as:

$$[010]_{\beta''} \parallel [001]_{\text{Al}} \ldots \ldots \text{growth direction},$$

$$[30\overline{2}]_{\beta''} \parallel (100)_{\text{Al}}.$$  

This relationship is also close to Andersen’s relationship,$^{16}$ i.e.,

$$[010]_{\beta''} \parallel [001]_{\text{Al}} \ldots \ldots \text{growth direction},$$

$$[001]_{\beta''} \parallel (100)_{\text{Al}}.$$  

In the alloy 6 aged at 300°C for 4 h, Type-A and B rods began to precipitate. The diameters of Type-A and B rods were as large as 100 nm and 10–30 nm, respectively. The examples are shown in Figs. 15 and 16. Figure 15(a) shows the bright field image containing both the Type-A and B rods. It can be seen that the diameter of Type-A rod is much larger than that of Type-B rod but the growth directions of both the rods are exactly the same, i.e., $[010]_{\text{Al}}$ direction. The orientation relationship between these rods and the matrix can be expressed as:

For Type-A rod:

$$[1\overline{2}10]_{\text{A}_1} \parallel [010]_{\text{Al}} \ldots \ldots \text{growth direction},$$

$$[0001]_{\text{A}_1} \parallel (301)_{\text{Al}}, (1010)_{\text{A}_1} \parallel (103)_{\text{Al}}.$$  

For Type-B rod:

$$[001]_{\text{B}} \parallel [010]_{\text{Al}} \ldots \ldots \text{growth direction},$$

$$[130]_{\text{B}} \parallel (100)_{\text{Al}}, (2\overline{1}0)_{\text{B}} \parallel (001)_{\text{Al}}.$$  

The Type-A/matrix orientation relationship is the same as that obtained above. The Type-B/matrix relationship is also very close to that obtained by Matsuda et al.,$^{11}$ i.e.,

$$[001]_{\text{B}} \parallel [010]_{\text{Al}} \ldots \ldots \text{growth direction},$$

$$(010)_{\text{B}} \text{ about } 20^\circ \text{ from } (100)_{\text{Al}}.$$  

In the alloy 6 aged at 300°C for 10 h. Arrow indicates $\beta'$ rod. (a) Bright field image and (b) the selected area electron diffraction pattern.
Fig. 13 Precipitation of Type-A rods in the excess Si alloy 5 aged at 210°C for 150 h. (a) Bright field image and (b) the selected area electron diffraction pattern.

Figures 16(a) and (b) are the bright field image and the selected area electron diffraction pattern from a different area in the same specimen. Although the variants of the orientation relationship are different from those in Fig. 15, the equivalent orientation relationships of both Type-A/matrix and Type/B/matrix were obtained. The precipitation of Type-C precipitates, however, could not be detected in the present experimental condition. Coarse Si particles were also clearly observed in the specimen aged at temperatures above 245°C for long time. An example in the alloy 6 aged at 300°C for 10 h is shown in Fig. 17. The bright field image and the selected area electron diffraction pattern are in Figs. 17(a) and (b), respectively. The morphology of the Si particle observed in (a) is quite similar to those observed by Matsuda et al., 20) and the edges of the polyhedral Si particle are parallel to the traces of {110}Al matrix planes as pointed out by Matsuda et al. The Si/Al orientation relationship determined from the diffraction pattern (b), however, can be expressed as:

\[(121)_\text{Si} \parallel (100)_\text{Al}, \quad (101)_\text{Si} \parallel (01\overline{1})_\text{Al}, \quad (101)_\text{Si} \parallel (031)_\text{Al}\]

and is different from that by Matsuda et al. 20) In the excess Si alloy 4 aged at 350°C for 4 h, the formation of platelike \(\beta\) has been observed. Figure 18 shows an example of a \(\beta\) plate exhibiting a different orientation relationship. In this case, the edges of the plate are parallel to \((100)_\text{Al} \parallel (110)_\beta\) directions and the relationship can be expressed as:

\[(100)_\text{Al} \parallel (110)_\beta, \quad (010)_\text{Al} \parallel (\overline{1}10)_\beta, \quad (001)_\text{Al} \parallel (001)_\beta\]

This is in good agreement with that reported previously. 7,8)

4. Discussion

In the previous continuous heating experiment, 18) the intermediate phases observed were limited, and the formation of Type-A and C rods could not be recognised. The phases precipitated during isothermal ageing processes are summarised in Table 2. Since age hardening is related to the precipitation processes, the relationship between hardness and the fine structures are examined.

As has been reported elsewhere, the maximum hardness is related to the amounts of \(\beta''\) needles and the average size of them. Since \(\beta''\) phase consists of Mg, Si and Al atoms, 9,11) the amounts of \(\beta''\) needles precipitated are thought to be dominated by the solubility product of Mg, Si and Al atoms and the increase of either Mg or Si atoms will increase the amounts of \(\beta''\) needles. The hardness, however, depends on the chemical composition in rather complicated manner. In order to compare the maximum hardness values, a complete solutionising of the precipitates is prerequisite. Thus, the chemical compositions were examined by the solubility limit curve for the stable \(\beta\)-Mg\(_2\)Si precipitates as shown in Fig. 1. It is interesting to note that the composition of the excess Mg alloy 2, which shows the peak hardness lower than that of the quasi-binary alloy 4, lies at a very critical region, indicating the possibility of the incomplete solutionising. The compositions of both the excess Si alloys 5 and 6 showing the peak hardness much higher than that of quasi-binary alloy 4, how-
ever, lie also in the region of incomplete solutionising. Thus, some other factors affecting the maximum hardness should be considered in addition to the incomplete solutionising. It should also be noted that in the excess Mg alloys cuboid \( \beta'\)-\( \text{Mg}_2\text{Si} \) particles precipitate separately at temperatures almost the same as those of \( \beta'' \) needles (Table 2). Therefore, when the undissolved \( \beta'\)-\( \text{Mg}_2\text{Si} \) particles exist, Mg and Si atoms in the \( \alpha \)-solid solution will migrate to the undissolved precipitates to grow them and will consume the amounts of free Mg and Si atoms quite easily during the precipitation of \( \beta'' \) needles, reducing the amounts of \( \beta'' \) needles. This may be the reason of the reduction of the maximum hardness in the excess Mg alloy 2.

On the other hand, in the excess Si alloys, the formation of cuboid \( \beta'\)-\( \text{Mg}_2\text{Si} \) particles is largely suppressed at temperatures where \( \beta'' \) needles precipitate (Table 2). This, in other words, implies that the undissolved \( \beta'\)-\( \text{Mg}_2\text{Si} \) particles are difficult to grow at \( \beta'' \) formation temperatures and excess Si atoms will enhance the precipitation of \( \beta'' \) needles even in the incomplete solutionising condition. Furthermore, the \( \beta'' \) needles contain large amounts of Si atoms, i.e., Si:Al:Mg = 6:3:1, as reported by Matsuda et al.\(^9, 11\) This will also accelerate the precipitation of \( \beta'' \) needles, resulting in the maximum hardness much higher than that if the quasi binary alloy even in the incomplete solutionising condition.

It should also be noted that the maximum hardness obtained in the excess Mg alloy 1 is much higher than that of the quasi-binary alloy 4 as can be seen in Figs. 2 and 3. In both the cases, the solution treatment temperatures were well within the \( \alpha \)-solid solution region, the difference existing in the vacancy concentration at the solutionising temperatures. If the vacancy clusters or the solute atom clusters which nucleated at vacancy clusters act as the nucleation sites for \( \beta'' \) needles, the density of them will be increased with raising the solution treatment temperature as in keeping with the experimental results.

The precipitation sequence is examined in the order of increasing ageing temperature. Since the precipitation of cuboid \( \beta'\)-\( \text{Mg}_2\text{Si} \) particles has been discussed in detail in

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**Table 2** The relationship between phases observed and ageing condition.

<table>
<thead>
<tr>
<th>Alloy</th>
<th>Temp (°C)</th>
<th>Ageing time (h)</th>
<th>( \beta'' ) (α) solid solution</th>
<th>( \beta'' ) (α) solid solution</th>
<th>( \beta'' ) (α) solid solution</th>
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<tr>
<td>Excess Mg</td>
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<td>1</td>
<td>10</td>
<td>100</td>
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<tr>
<td></td>
<td>210</td>
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<td>( \beta'' ) (α) solid solution</td>
<td>( \beta'' ) (α) solid solution</td>
<td>( \beta'' ) (α) solid solution</td>
</tr>
<tr>
<td></td>
<td>300</td>
<td>Not examined</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
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<td>Quasi-binary Mg</td>
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<td></td>
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<td>210</td>
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<td>( \beta'' ) (α) solid solution</td>
<td>( \beta'' ) (α) solid solution</td>
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<tr>
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<td>300</td>
<td>Not examined</td>
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<td>350</td>
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</tr>
<tr>
<td>Excess Si</td>
<td>185</td>
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<td>1</td>
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<tr>
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<td>210</td>
<td>30min</td>
<td>( \beta'' ) (α) solid solution</td>
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\( \beta'' \) needles, c-β: cuboid \( \beta \) particles, \( \beta' \): \( \beta'' \) needles, \( \beta'' \): cuboid \( \beta \) particles and \( \beta' \) plates, \( \beta' \): \( \beta' \) rods, A: Type-A rods, B: Type-B rods, Si: Si particles, MH: the ageing time showing the maximum hardness.
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Fig. 17 Precipitation of Si particles in the excess Si alloy 6 aged at 300°C for 10 h. (a) Bright field image and (b) the selected area electron diffraction pattern.

the previous studies,8,18) the formation of other intermediate phases is examined here. In the excess Si alloys, Type A rods starts to precipitate after β'' needles and fine Si particle formation at 210°C. The average diameter of Type-A rods is extremely thick, i.e., 80–100 nm. The fact that Type-A rods precipitate easily at temperatures as low as 210°C implies that they form without large partition of solute atoms. This is because the nucleation and growth depend largely on the solute atom diffusion. It has been reported by Matsuda et al.9,11) that the chemical composition of β'' phase is Si:Al:Mg = 6:3:1 and that of Type-A phase is Si:Al:Mg=5:4:1. Therefore, if some β'' needles transform into Type-A rods with absorbing Al atoms from the adjacent Al matrix in-situ fashion, the growth of Type-A will be achieved by small partition of alloying elements. Considering that the growth direction and the interplanar spacing of (020)β'' for β'' needles16) are [010]β'' || (001)Al and 0.2025 nm, and that the growth direction and the interplanar spacing of (1210)A for Type-A rods10) are [1210]A || (001)Al and 0.2025 nm, respectively, it is likely that the in-situ transformation occurs. This may be the reason that such a coarse Type-A rod can precipitate at temperatures as low as 210°C. It should be noted that cuboid β particles do not precipitate after β'' precipitation in the excess Si alloys isothermally aged at 210°C although the precipitation reactions described above occur. This is a quite large difference from the precipitation sequence during the continuous heating.8)

At 245°C, although the ageing processes in the excess Mg and the quasi-binary alloys are accelerated significantly in comparison with those at 210°C, the precipitation sequences are basically the same. In the quasi-binary alloy, it has so far been believed that the reaction occurring immediately after β'' precipitation is the precipitation of β' rods. In the previous study, however, it was confirmed that the reaction after β'' precipitation is the precipitation of cuboid β particles.8) This result is in keeping with the present isothermal ageing result as far as the excess Mg and the quasi-binary alloys are concerned. It should be noted that β' rods precipitate at quite later stage of ageing after the formation of cuboid β particles in the excess Mg alloy and the quasi-binary alloys. But the ageing sequence in the excess Si alloys is different and quite similar to that of the ageing at 210°C.

In the case of ageing at temperatures 300–350°C, the reactions are much accelerated in the excess Mg and the quasi-binary alloys but those for the excess Si alloys are significantly different from the reactions in the alloys aged at temperatures below 245°C. By ageing at these temperatures, Type-B and β' rods form in addition to Type-A rods. It is interesting to note that the precipitation sequence of rod-like precipitates in the excess Si alloys is: coarse Type-A rods → relatively thin Type-B rods → relatively thin β' rods. Such a sequence can be understood by considering the
chemical compositions of the intermediate phases determined by Matsuda et al., i.e., Si:Al:Mg = 5:4:1 for Type-A,\(^9,11\) Si:Al:Mg = 5:4:2 for Type-B\(^10,11\) and Si:Al:Mg = 1:0:2 for \(\beta’\) rods.\(^{11,19,21}\) It is only necessary for the formation of Type-A rods from \(\beta''\) needles to absorb small amounts of Al atoms from the matrix as described above. In the case of Type-B precipitation from \(\beta''\) needles, some additional Mg atoms should be absorbed. For the formation of \(\beta'\) rods, complete re-partition of the chemical composition is prerequisite because \(\beta'\) phase does not contain Al atoms with Mg\(_2\)Si composition. The precipitation sequence determined in the present study, however, is contradict with that obtained by Matsuda et al.,\(^2\) i.e., \(\beta'\) rods\(\rightarrow\)Type-B rods\(\rightarrow\)Type-A in their study. Although the reason for it is not clear at present, it may arise from the difference in either the chemical composition or the ageing temperature. It should, however, be noted that the present sequence seems much reasonable in view of the compositions of the intermediate phases determined by Matsuda et al. Type-C rods could not be detected in the present alloys.

5. Conclusions

The effects of excess Mg and Si contents on the isothermal ageing processes of Al–Mg\(_2\)Si alloys have been investigated mainly by means of transmission electron microscopy. The precipitation behaviours observed were largely different from those recognised during continuous ageing at a constant heating rate. The results are summarised as follows.

(1) Large age hardening arises from the precipitation \(\beta''\) needles as has been reported so far.

(2) After the formation of \(\beta''\) needles, cuboid \(\beta\) particles precipitate and the following reaction is the precipitation of \(\beta'\) rods and then \(\beta\) plates form in the excess Mg and the quasibinary alloys, but fine Si particles nucleate in the excess Si alloys.

(3) In the excess Si alloys, rodlike precipitates form after the precipitation of both \(\beta''\) needles and Si particles in the sequence as: coarse Type-A rods\(\rightarrow\)relatively thin Type-B rods\(\rightarrow\)relatively thin \(\beta'\) rods. This precipitation sequence can be understood by considering the chemical compositions of them determined by Matsuda et al.\(^9,11,18,21\)

(4) The orientation relationships between these interme-
diate phases and the \(\alpha\) matrix are in good agreement with those reported so far.

(5) Two types of Si/\(\alpha\) matrix orientation relationships different from that obtained by Matsuda et al.\(^2\) were determined.

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