Simulation on Sawtooth Period Control in Tokamak Plasma

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The sawtooth period control is important in inductive operation of tokamak plasma because the sawteeth with long periods trigger the neoclassical tearing modes (NTMs) which reduce the plasma confinement capability significantly. We studied the effect of the sawtooth period control by the electron cyclotron current drive (ECCD) in ITER using the 1.5-dimensional transport code TOTAL. There is the optimum condition (CD direction and radial position) of ECCD for minimizing the sawtooth period. In addition, it was found that the optimum condition hardly depends on the total external heating power from 50 MW to 110 MW and the driven current from 0.5 MA to 1.0 MA. The effect of the sawtooth period control on the critical normalized beta for triggering NTMs was investigated, and it was found that the critical normalized beta increases according to increase in the driven current and ECCD can increase the margin of the normalized beta.

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1. Introduction

In inductive operation of tokamak plasma such as the standard operation of ITER, the safety factor at the center of plasma becomes below unity through penetration of the plasma current, so that the sawtooth oscillation occurs in the central region of plasma. The sawteeth eject plasma stored energy from the plasma center and limit the fusion power. Furthermore, the sawteeth with long periods may trigger other plasma instabilities such as the neoclassical tearing modes (NTMs) [1, 2]. NTMs reduce the plasma confinement capability significantly. Therefore, it is necessary to shorten the sawtooth period so as to not to trigger NTMs for achieving a high performance. Using the feature that onset conditions of the sawtooth crashes depend on the magnetic shear at the $q = 1$ radius [3], the sawtooth period control is attempted by changing the magnetic shear at the $q = 1$ radius using the electron cyclotron current drive (ECCD).

We studied the effect of the sawtooth period control by the electron cyclotron current drive (ECCD) in ITER using the 1.5-dimensional transport code TOTAL (toroidal transport analysis linkage) [4]. $\chi^{AN}$ is the anomalous part. For $\chi^{AN}$, we used the mixed Bohm/gyro-Bohm model [5]. The Porcelli model [6,7] is used as the triggering sawtooth model. In this model, the sawtooth crashes are triggered when one of the three conditions is satisfied. The condition (1) means that the fast ion stabilization doesn’t work within a time scale of mode growth. The condition (2) means that the driving force overcomes the diamagnetic rotation stabilization of thermal ions. The condition (3) means that the resistive internal kink mode is driven for potential energy change close to zero. The full reconnection model is used for the profile after the sawtooth crash. The full reconnection model is a simple model that the magnetic surfaces reconnect within the mixing radius in the Kadomtsev model [6,8].

As a localized current drive model, we adopted ECCD with a Gaussian function $j_{CD}$ which is given by

$$j_{CD}(\rho) \propto \exp[-((\rho - \rho_{CD})/w)^2].$$

(1)

where $\rho$ is the normalized minor radius, $\rho_{CD}$ is the normalized radius of position of ECCD and $w$ is the half width for 1/e of the peak value. The driven current $I_{CD}$ is given by

$$I_{CD} = \int_S j_{CD}(\rho) dS,$$

(2)

where $S$ is the plasma poloidal cross section. ECCD was applied to change the magnetic shear at the $q = 1$ radius. We kept $\rho_{CD}$ constant in time for simple control logic. We adopted $0.2 \times 10^{20}$ Am^{-2} W^{-1} [9] for the driven current efficiency in order to calculate the ECCD power $P_{CD}$.

The critical $\beta_S$ for triggering NTMs depends on the sawtooth period. The following empirical scaling of

$$\beta_S \propto \frac{1}{T_{95}} \exp\left[-\frac{\rho_{CD}}{\rho_T}\right],$$

(3)

where $\rho_T$ is the characteristic radius for triggering NTMs.
the critical $\beta_N$ for triggering NTMs was derived from a database of plasma parameters with the sawtooth crashes which trigger NTMs and do not [2].

$$\rho_N^{\text{NTM}} = 2.614 \left( \frac{\tau_{\text{saw}}}{\tau_r} \right)^{0.4084} \rho_0^{0.5721} \left( \frac{P_{\text{aux}}}{P_{\text{LH}}} \right)^{0.4204} \times \bar{n}_e \left[ 10^{19} \text{m}^{-3} \right]^{0.4948},$$

where $\rho_N^{\text{NTM}}$ is the critical $\beta_N$ at which the sawtooth crashes will trigger NTMs, $\tau_{\text{saw}}$ is the sawtooth period, $\tau_r$ is the resistive diffusion time at the $q = 1$ radius, $\rho_0$ is the poloidal ion Larmor radius at the $q = 1$ radius normalized by the minor radius of the $q = 1$ surface, $P_{\text{aux}}$ is the auxiliary heating power, $P_{\text{LH}}$ is the L-H threshold power and $\bar{n}_e$ is the line average electron density.

The external heating except for ECCD is assumed to be simply given by a profile of $\exp\left(-\left(\rho/0.6\right)^2\right)$ with the power of $P_{\text{ext}}$. The total external heating power $P_{\text{total}}$ is the sum of $P_{\text{CD}}$ and $P_{\text{ext}}$. We used the standard operation parameters of ITER for the plasma parameters, which are shown in Table 1. The edge temperature is set to be 3 keV so that $HHy_2 \approx 1$ is obtained with $P_{\text{total}} = 73$ MW, which is the total external heating power in ITER. In this condition, the fusion power $P_{\text{fusion}}$ calculated by TOTAL code is 463 MW. In addition, $HHy_2 \approx 0.99$, $\beta_N = 2.06$ and $P_{\text{fusion}} = 453$ MW when $P_{\text{total}} = 50$ MW. In this case, the fusion gain ($Q$) is about 9.1 which is close to the ITER reference value ($Q = 10$ for $HHy_2 = 1$).

### 3. Simulation Results

#### 3.1 The optimum ECCD direction and position for the minimum sawtooth period

In this subsection, we investigate how the sawtooth period normalized by the resistive diffusion time $\tau_{\text{saw}}/\tau_r$ changes when the direction and the radial position of ECCD are changed on the conditions that the total external heating power $P_{\text{total}}$ is 73 MW, $I_{\text{CD}}$ is 0.65 MA and $w$ is 0.06. The 0.65 MA is obtained assuming that the ECCD efficiency is $0.2 \times 10^{20} \text{Am}^{-2} \text{W}^{-1}$ and the ECCD power is 20 MW which is the ECCD power in ITER.

Figure 1 shows dependence of $\tau_{\text{saw}}/\tau_r$ on the ECCD position where the ECCD direction is in the same direction as the plasma current (co-ECCD) or counter to it (ctr-ECCD). The sawtooth crash is triggered by lowering the magnetic shear at the $q = 1$ radius. The minimum $\tau_{\text{saw}}/\tau_r$ is obtained by co-ECCD at $\rho_{\text{CD}} = 0.57$. The minimum value is smaller than that without ECCD by about 33%. Figure 2 shows the profiles of the safety factor, the magnetic shear and the EC-driven current density before a sawtooth crash. The dash lines denote the case without ECCD and the solid lines denote the case with (a) co-ECCD or (b) ctr-ECCD.

### Table 1 Standard operation parameter of ITER.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
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<tr>
<td>$R$ [m]</td>
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<tr>
<td>$a$ [m]</td>
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</tr>
<tr>
<td>$B$ [T]</td>
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<tr>
<td>$I_p$ [MA]</td>
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</tr>
<tr>
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<tr>
<td>$\delta$</td>
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</tr>
<tr>
<td>$\bar{n}_e$ [m$^{-3}$]</td>
<td>$1.0 \times 10^{20}$</td>
</tr>
</tbody>
</table>
dius before the sawtooth crash, than without ECCD. Thus the sawtooth crash is triggered and the sawtooth period becomes short. The ctr-ECCD can also shorten the sawtooth period. This is because ctr-ECCD increases the magnetic shear at the current drive positon and decreases it outside, as shown in Fig. 2 (b). However, decrease in the magnetic shear at the $q = 1$ radius by ctr-ECCD is smaller than that by co-ECCD, so co-ECCD is more effective to shorten the sawtooth period.

We also investigate the optimum ECCD direction and position in other total external heating and current drive conditions. Figure 3 shows dependence of $\tau_{saw}/\tau_r$ on $\rho_{CD}$ for different $P_{total}$ (50 MW and 110 MW) with fixed $I_{CD}$ (0.65 MA). The 110 MW is the total external heating power expected in ITER after upgrade in the future [10]. According to Fig. 3, it is found that the $\tau_{saw}/\tau_r$ is minimized by co-ECCD at $\rho_{CD} = 0.57$, which is the same as the case that $P_{total}$ is 73 MW and $I_{CD}$ is 0.65 MA, so the optimum ECCD direction and position do not change for $P_{total}$ between 50 MW and 110 MW. Figure 4 shows dependence of $\tau_{saw}/\tau_r$ on $\rho_{CD}$ for different $I_{CD}$ (0.5 MA and 1.0 MA) with fixed $P_{total}$ (73 MW). The 1.0 MA of EC-driven current is expected for the ECCD power of 31 MW, which is obtained assuming that the ECCD power is about 1.5 times larger than that 20 MW in the future as well as the total external heating power. According to Fig. 4, the $\tau_{saw}/\tau_r$ has its minimum at $\rho_{CD} = 0.57$ for $I_{CD}$ with 0.5 MA. On the other hand, the $\tau_{saw}/\tau_r$ has its minimum at $\rho_{CD} = 0.56$ for $I_{CD}$ with 1.0 MA, but the difference of $\tau_{saw}/\tau_r$ between $\rho_{CD} = 0.56$ and $\rho_{CD} = 0.57$ is about 8 %, so it can be said that the optimum ECCD direction and position do not change for $I_{CD}$ within 1.0 MA. Therefore, the optimum ECCD direction and position hardly change within the range of the total external heating power and the driven current expected in ITER.

3.2 Effect of the sawtooth period control on the onset of NTMs

In this subsection, we investigate $\beta_{NTM}^N$ when the sawtooth period is controlled. According to subsection 3.1, we applied co-ECCD with $w = 0.06$ on $\rho_{CD} = 0.57$. We considered three cases of $P_{total} = 50, 73, 110$ MW, and $I_{CD}$ is changed in each case.

Figure 5 shows dependence of $\tau_{saw}/\tau_r$ and $\beta_{NTM}^N$ on $I_{CD}$. The higher $I_{CD}$ is, the larger the effect of ECCD is. Table 2 shows values of $\tau_{saw}/\tau_r$, $\beta_{NTM}^N$, $\beta_N$ and the margin of $\beta_N$ ($\beta_{N\text{margin}}$), which is defined as $\beta_{N\text{margin}} = 100(\beta_{NTM}^N/\beta_N - 1)$, in the case without ECCD and the case with ECCD ($I_{CD} = 0.65$ MA) on different total external heating power. According to Table 2, though the possibility that the sawtooth crash triggers NTMs is small even without ECCD, ECCD can shorten $\tau_{saw}/\tau_r$ by about 33~37 % and increase $\beta_{NTM}^N$ by about 19~22 % for $I_{CD}$ of 0.65 MA. On the other hand, $\beta_N$ hardly change with ECCD, so $\beta_{N\text{margin}}$ can be increased by about 40~50 % when the sawtooth period is shortened by ECCD. Therefore, it is
4. Summary

For investigating the effect of the sawtooth period control by ECCD, we evaluated the sawtooth period normalized by the resistive diffusion time and the critical normalized beta for the sawteeth to trigger NTMs on various conditions for standard operation parameters of ITER.

There is the optimum ECCD condition (co-direction to the plasma current and the position slightly outside the \( q = 1 \) surface) and it hardly changes when the total external heating power is changed from 50 MW to 110 MW or the driven current is changed from 0.5 MA to 1.0 MA.

The possibility that the sawtooth crash triggers NTMs is small even without ECCD in ITER. On the other hand, higher ECCD current with the optimum condition makes the sawtooth period shorter and the critical normalized beta higher, so it is possible to make the plasma which has the high margin of triggering NTMs.

According to this study, it is confirmed that ECCD with the optimum condition is effective for the sawtooth period control and preventing the sawteeth from triggering NTMs.

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